

Modeling and Analysis of Fixturing Dynamic Stability in Machining

Haiyan Deng, Ph.D. Candidate

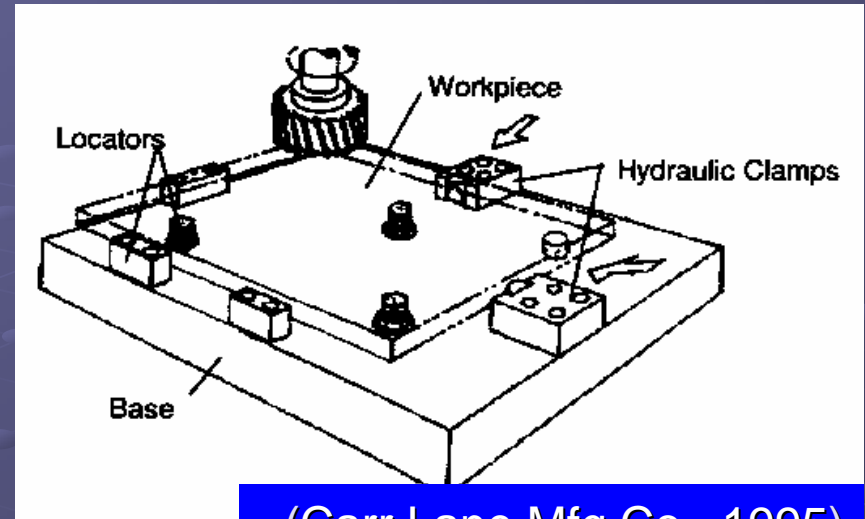
Precision Machining Research Consortium (PMRC)
George W. Woodruff School of Mechanical Engineering
Georgia Institute of Technology
Atlanta, Georgia, USA

Advisor: **Prof. Shreyes N. Melkote**

Introduction

Machining Fixture:

- Establish and maintain required position and orientation of a workpiece
- Directly affects operational safety and part quality



(Carr Lane Mfg Co., 1995)

Limitations of Previous Work:

- Majority ignores system dynamics, e.g., inertia, damping, material removal effect
- No information available on experimental investigation of fixture-workpiece dynamics during machining
- No information available on optimization of fixture-workpiece dynamics

Objectives

- Establish a mathematical procedure to analyze dynamic stability of a fixtured workpiece in machining
- Model and investigate material removal effect on system dynamic behavior
- Optimize fixture design to achieve fixturing dynamic stability
- Quantify and synthesize dynamics-induced part quality errors
- Run machining experiments to validate and refine models

Stability Analysis – Criteria

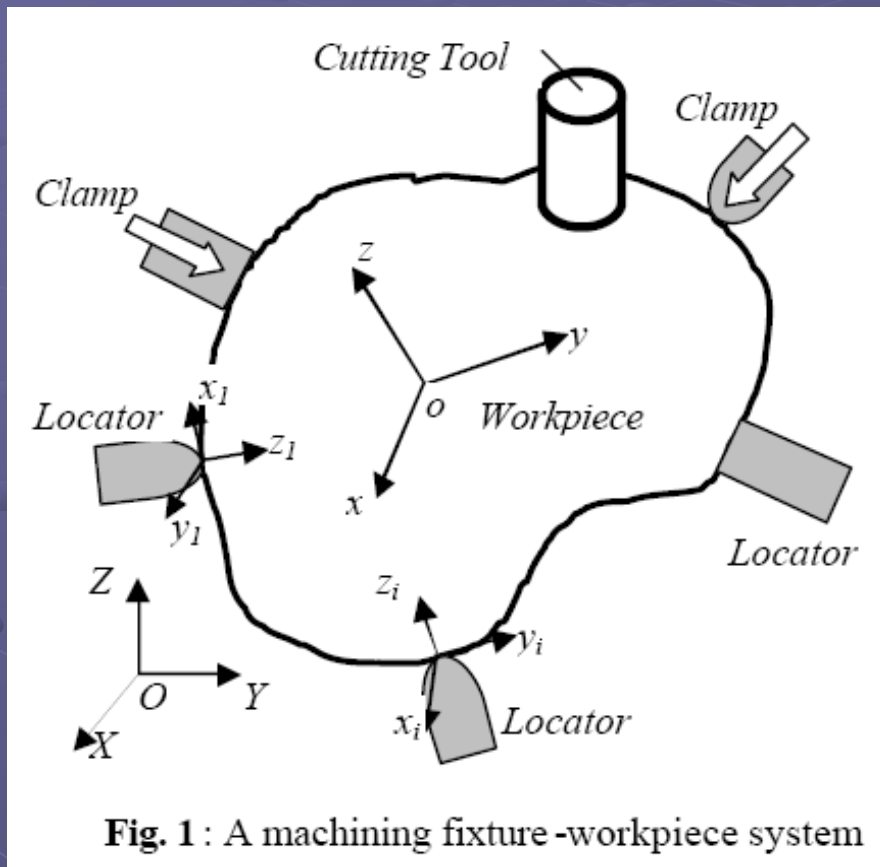
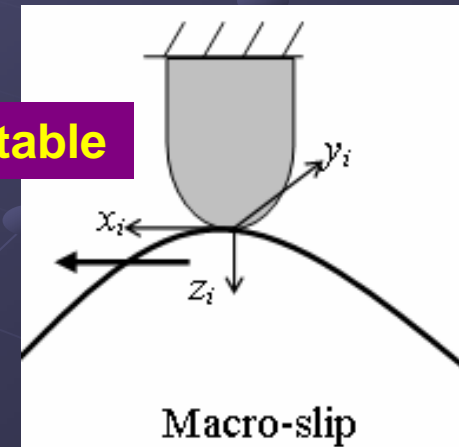
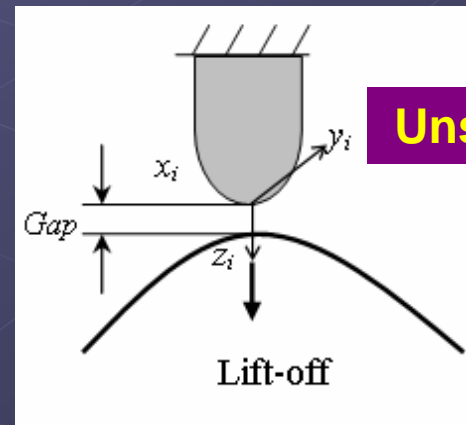
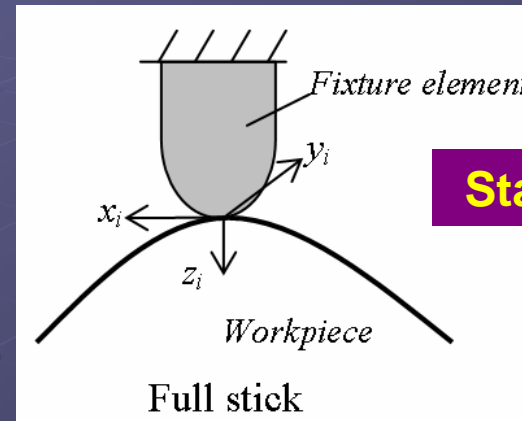
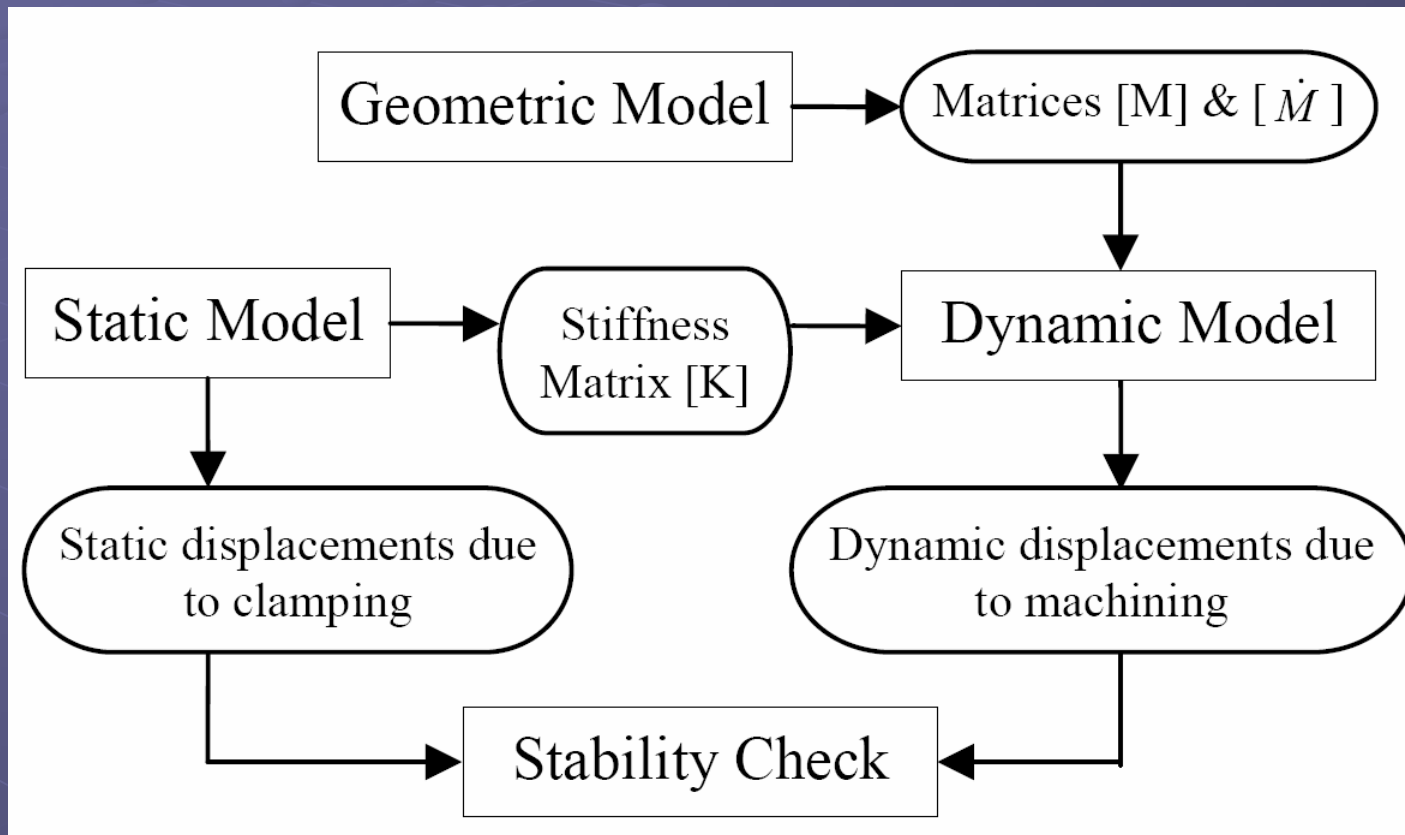


Fig. 1 : A machining fixture-workpiece system



Stability Analysis – Procedure



Stability Modeling

Minimize $\Pi_C(P_i, Q_{xi}, Q_{yi})$
 P_i, Q_{xi}, Q_{yi}

Subject to:

$$\sum \bar{F} = \bar{0}, \quad \sum \bar{M} = \bar{0}$$

$$P_j = F_{ej}$$

$$\sqrt{(Q_{xi})^2 + (Q_{yi})^2} - \mu_s^i P_i \leq 0$$

$$P_i \geq 0$$

$$P_i - S_y(\pi a_i^2) \leq 0$$

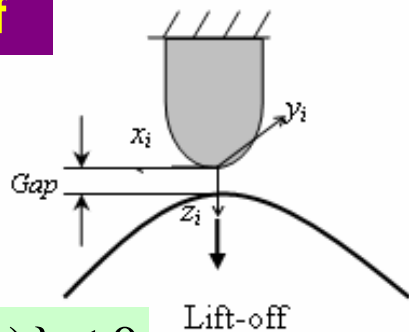
$$[M] \ddot{\bar{q}} + [\dot{M}] \dot{\bar{q}} + [K] \bar{q} = \bar{Q}(t)$$

**Clamping
Statics**

**Machining
Dynamics**

**Fixturing
Stability**

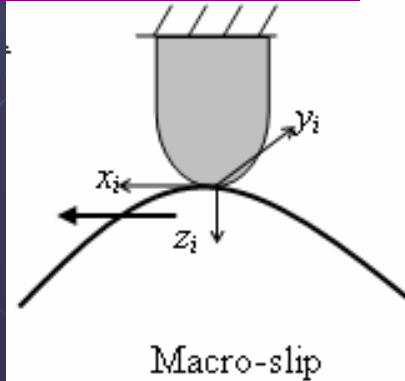
Lift-off



$$\max_t \{\Delta_{zi}(t)\} \leq 0$$

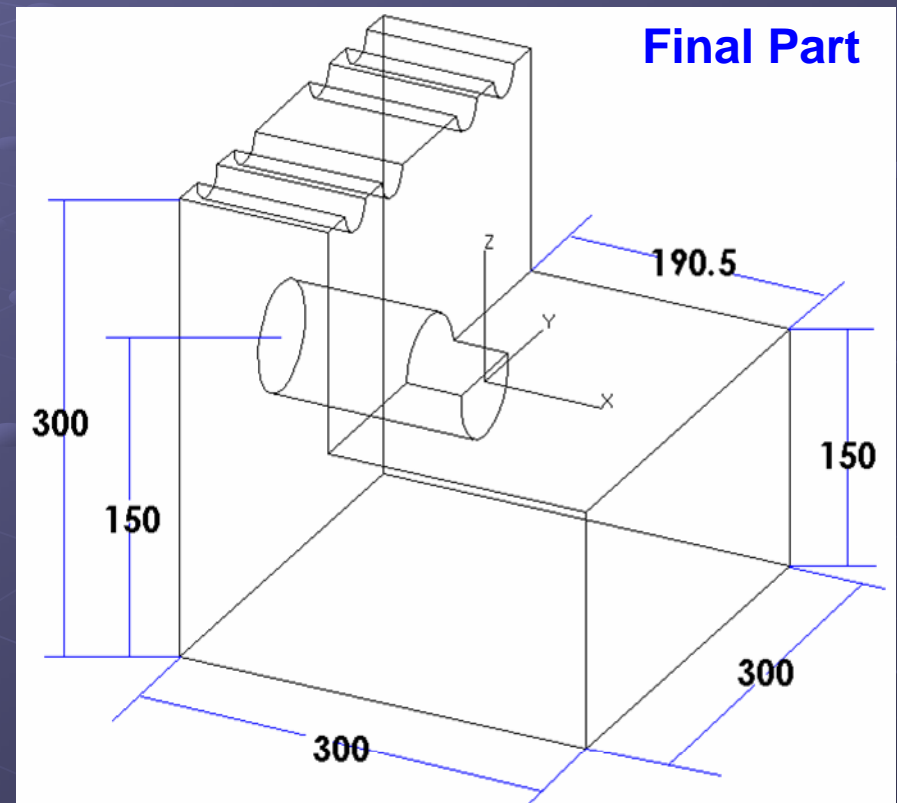
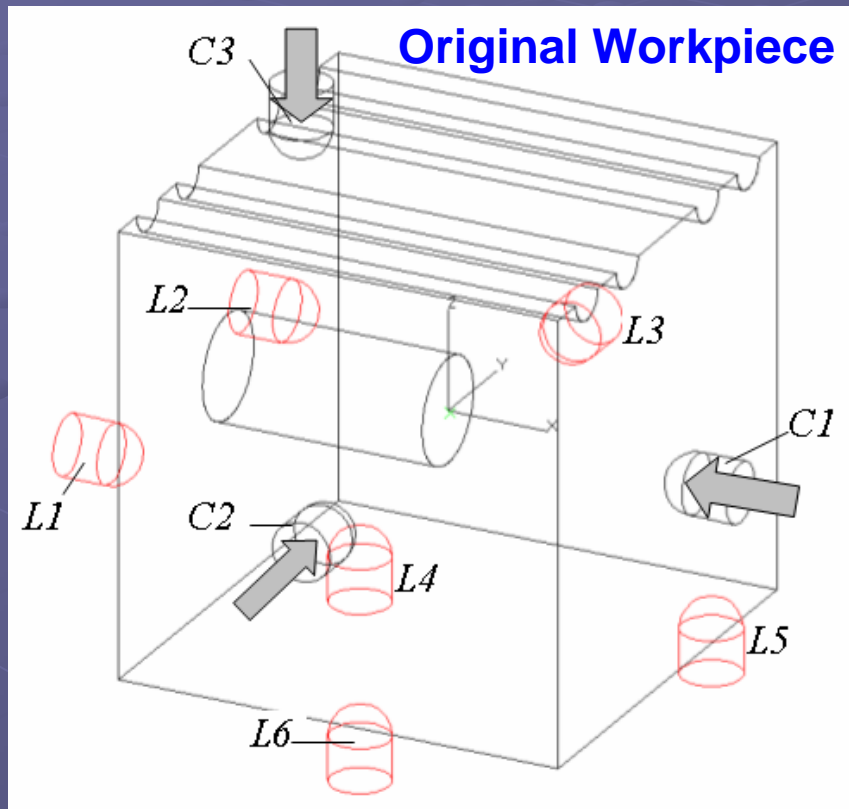
$$\Delta_{ji}(t) = d_{ji}(t) - \delta_{ji}$$

Macro-slip



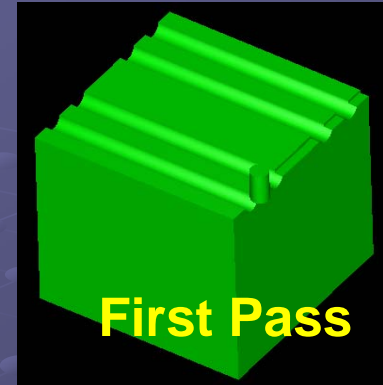
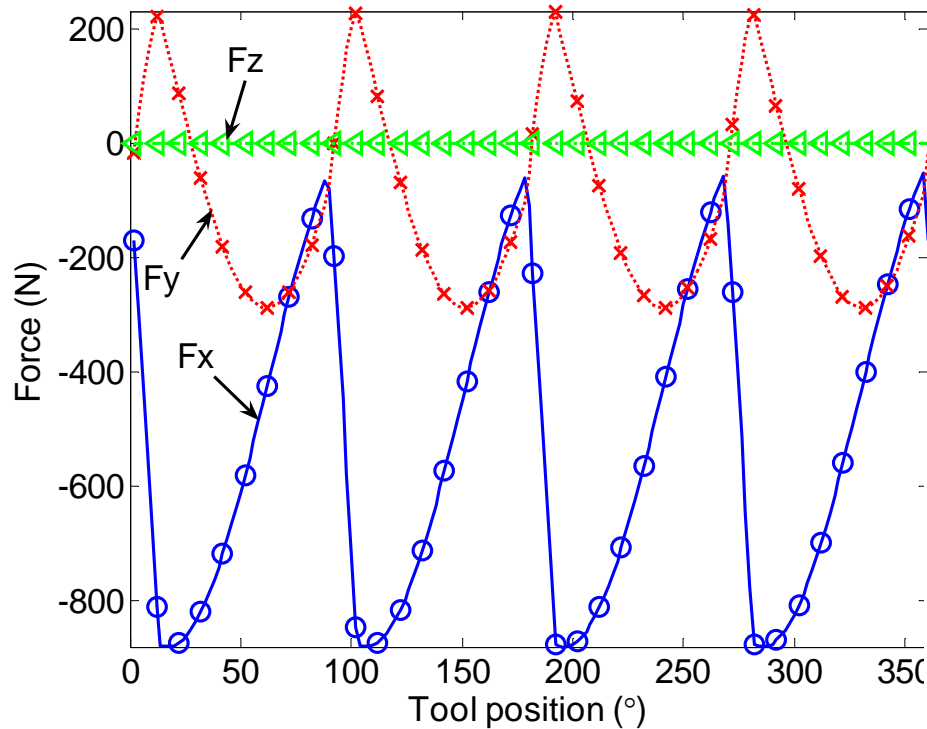
$$\max_t \{ \sqrt{[k_{xi} \Delta_{xi}(t)]^2 + [k_{yi} \Delta_{yi}(t)]^2} - \mu_s^i [k_{zi} |\Delta_{zi}(t)|] \} \leq 0$$

Simulation Example (1)

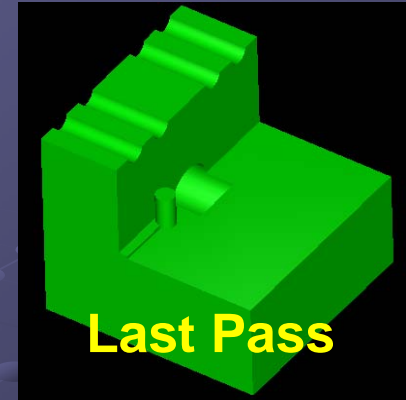


Simulation Example (2)

Cutting Forces

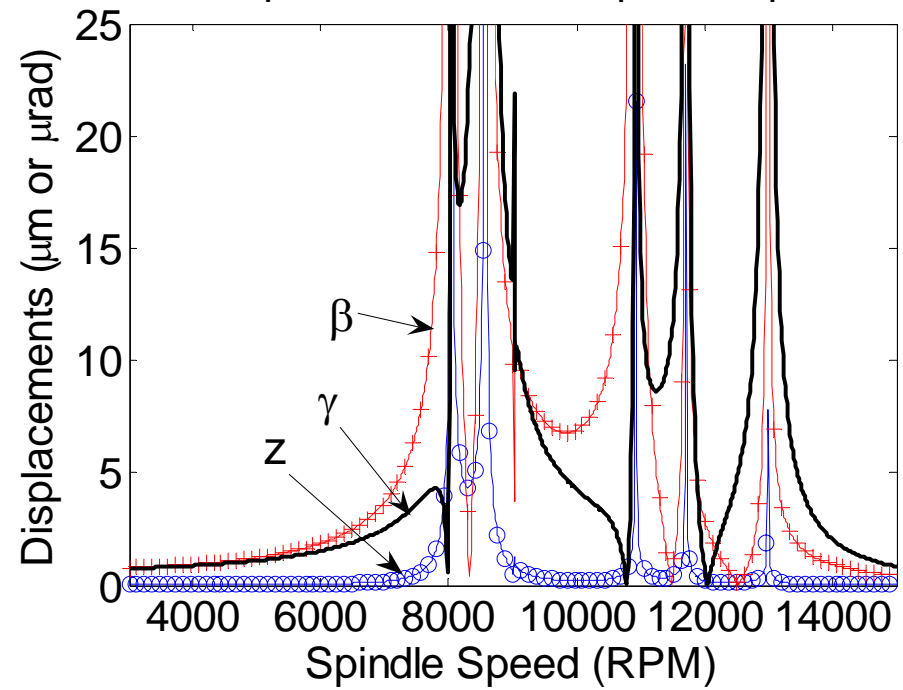


First Pass

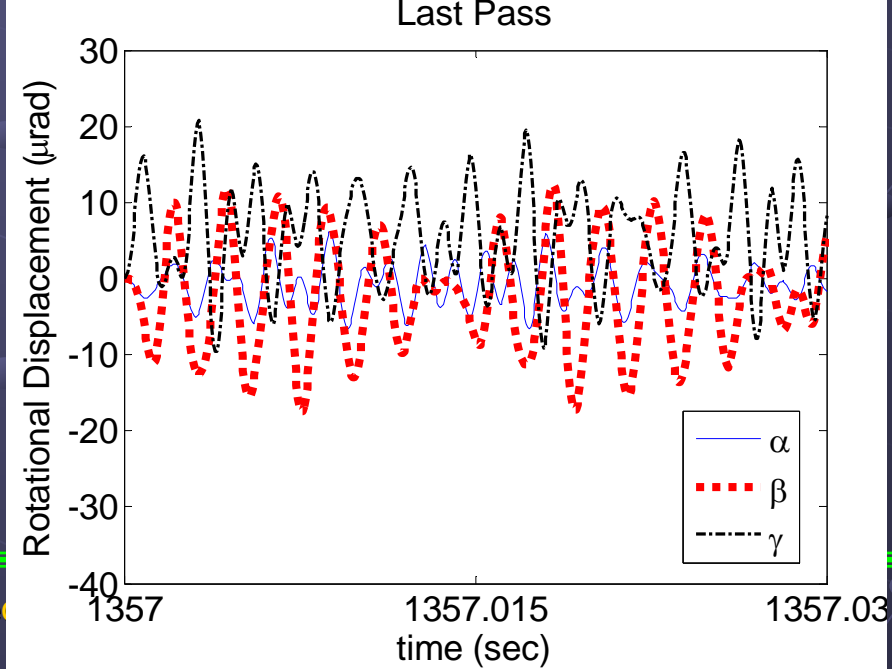
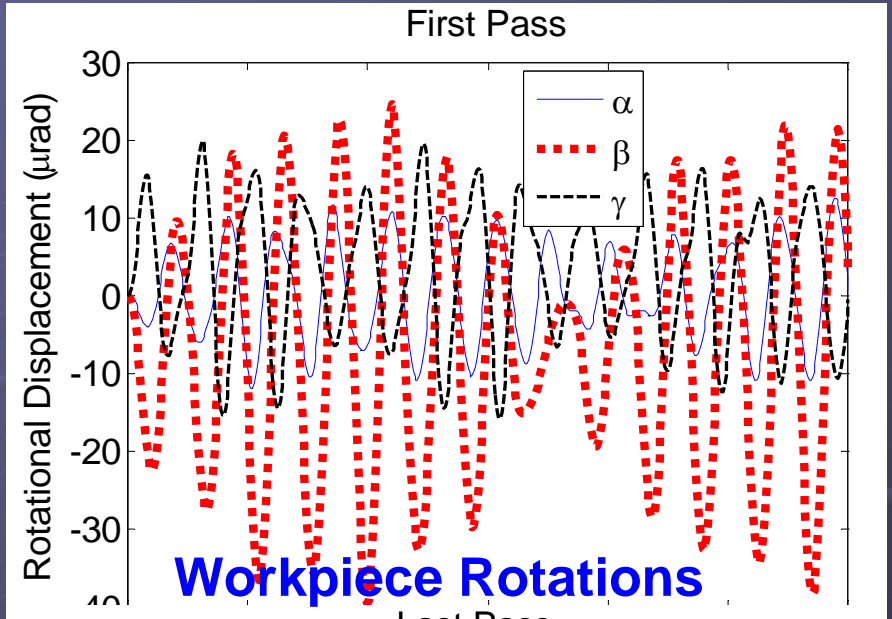
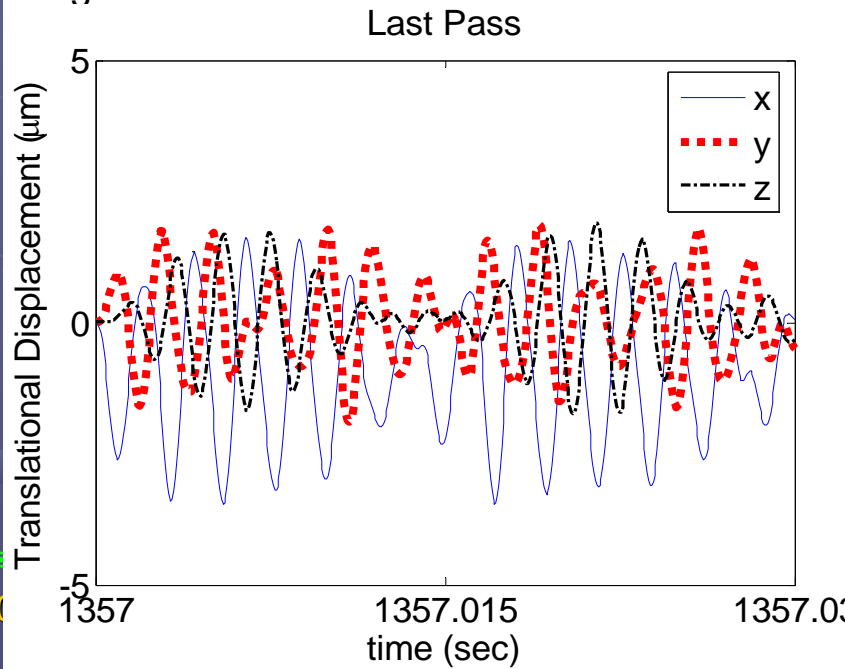
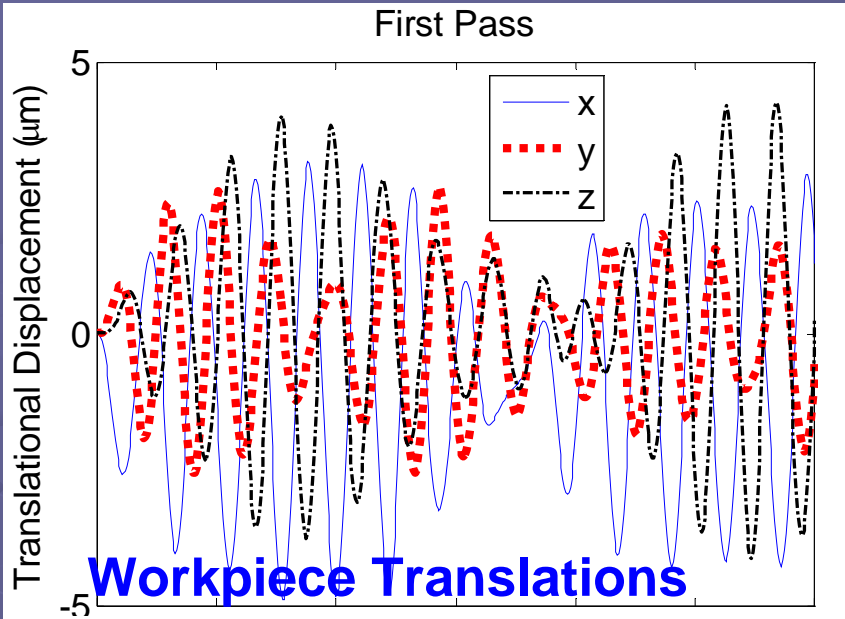


Last Pass

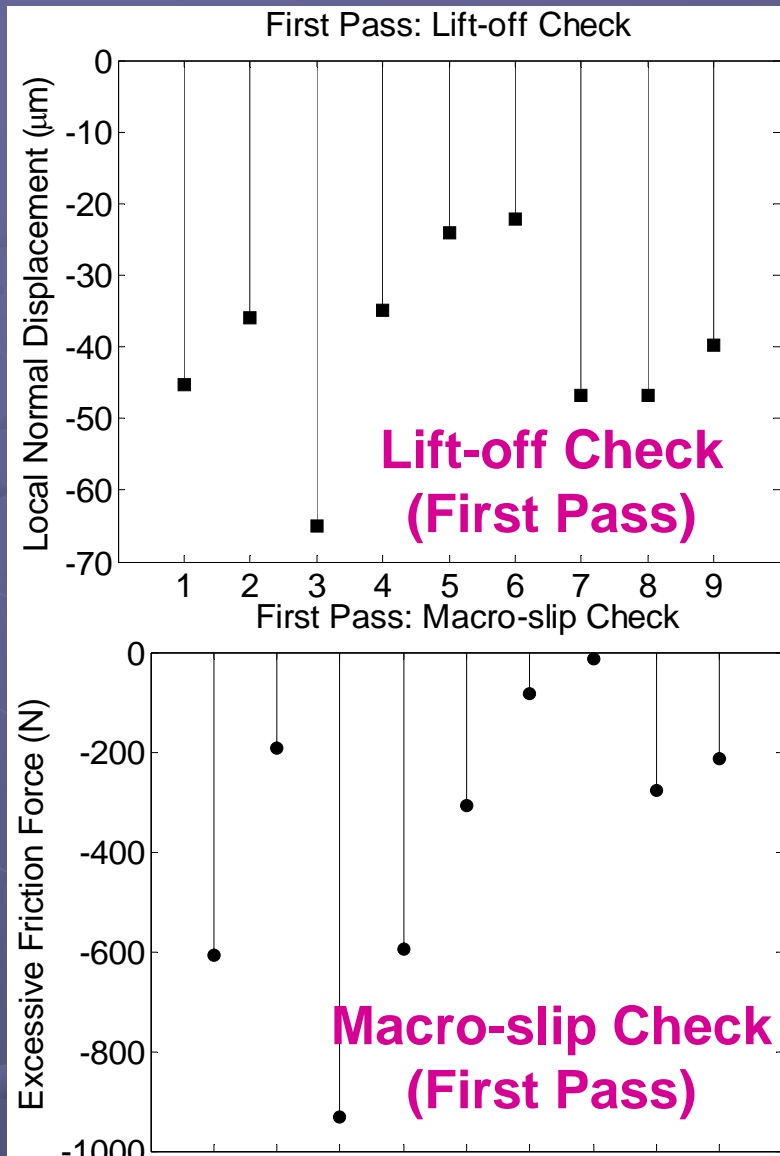
Workpiece Motion vs. Spindle Speed



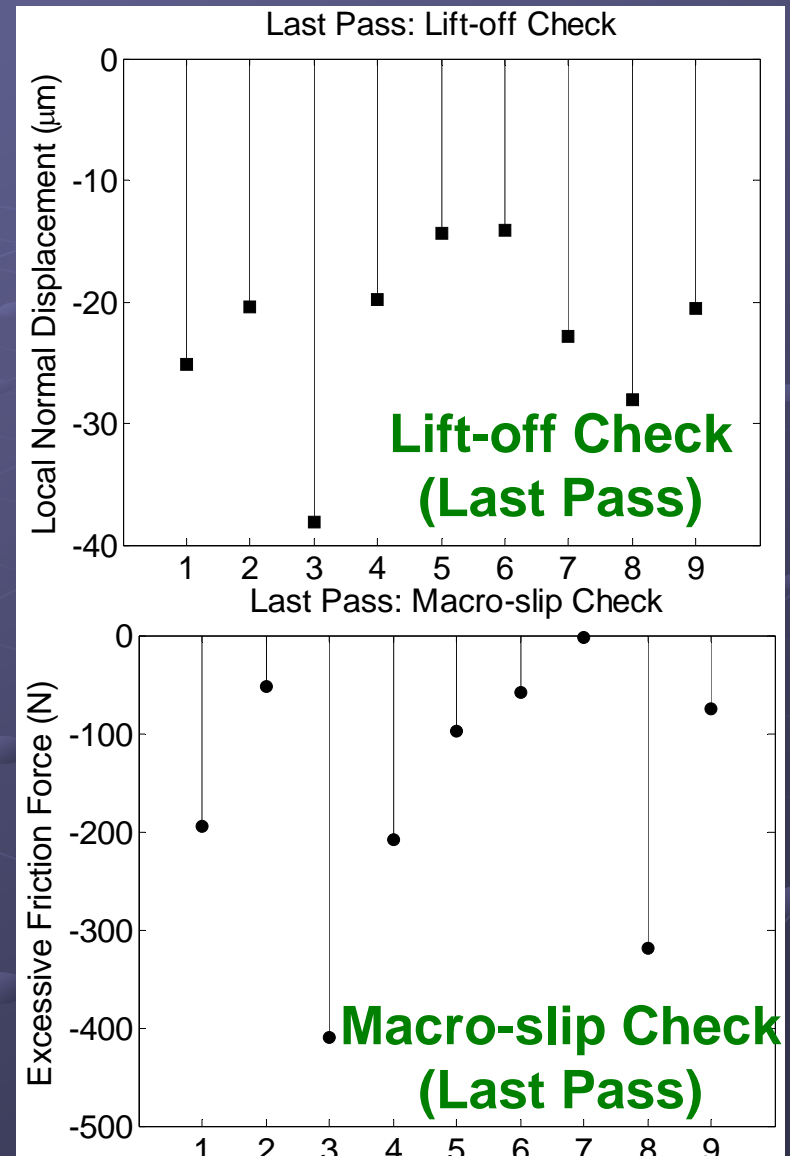
Simulation Example (3)



Simulation Example (4)



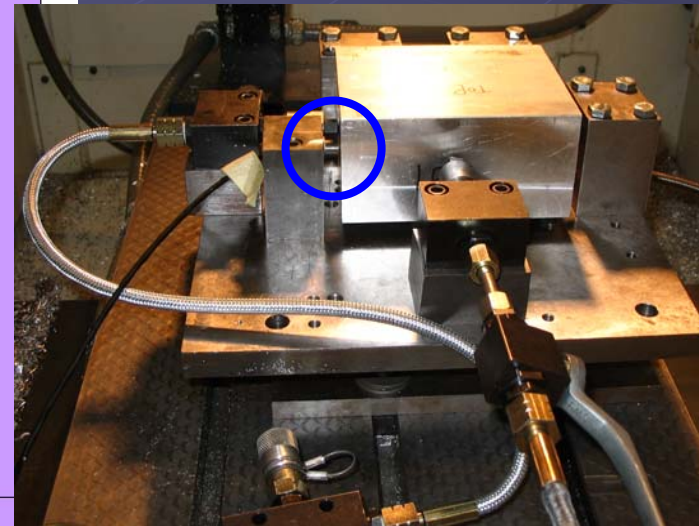
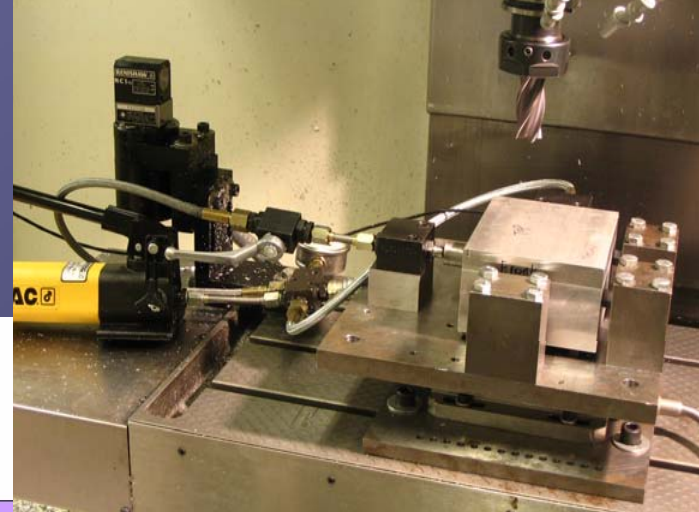
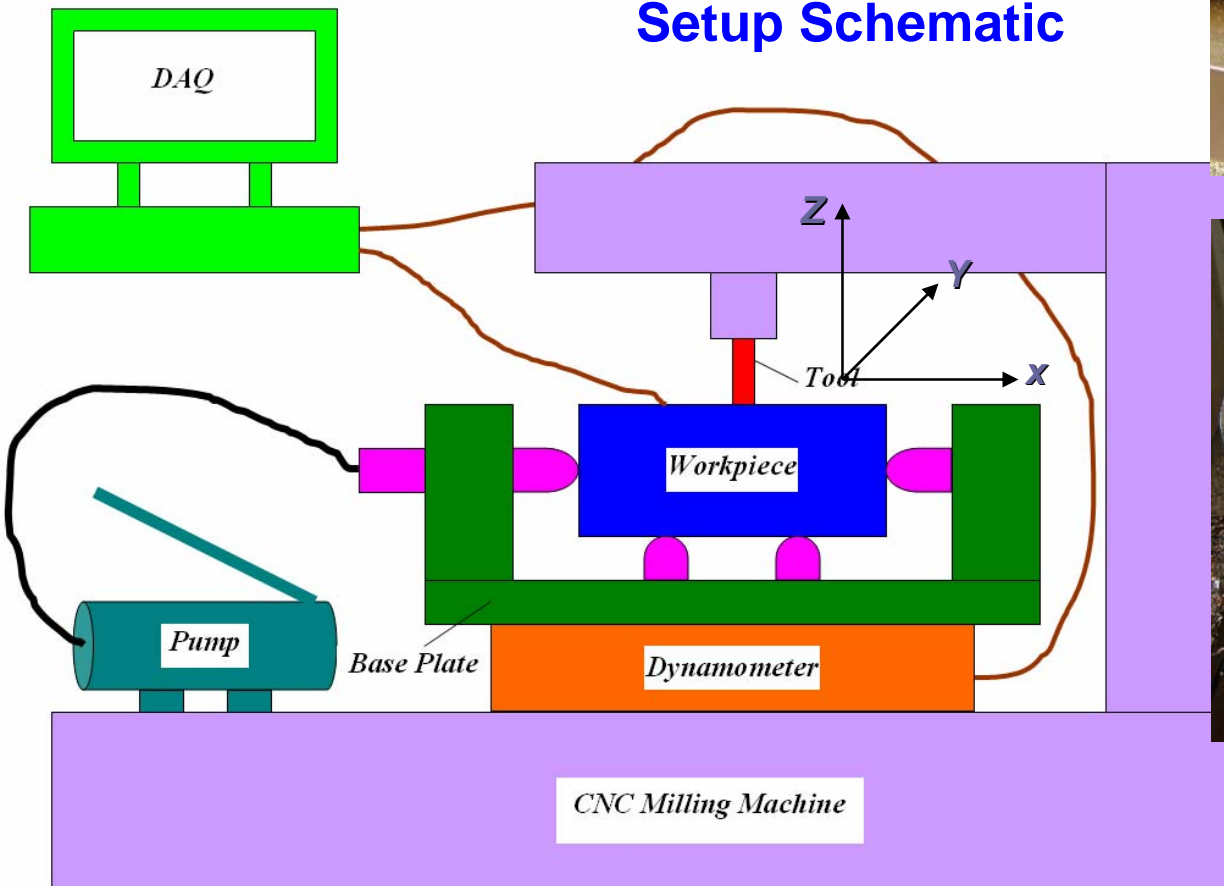
$FC = [5261.3, 2864.4, 3310.1] \text{ (N)}$



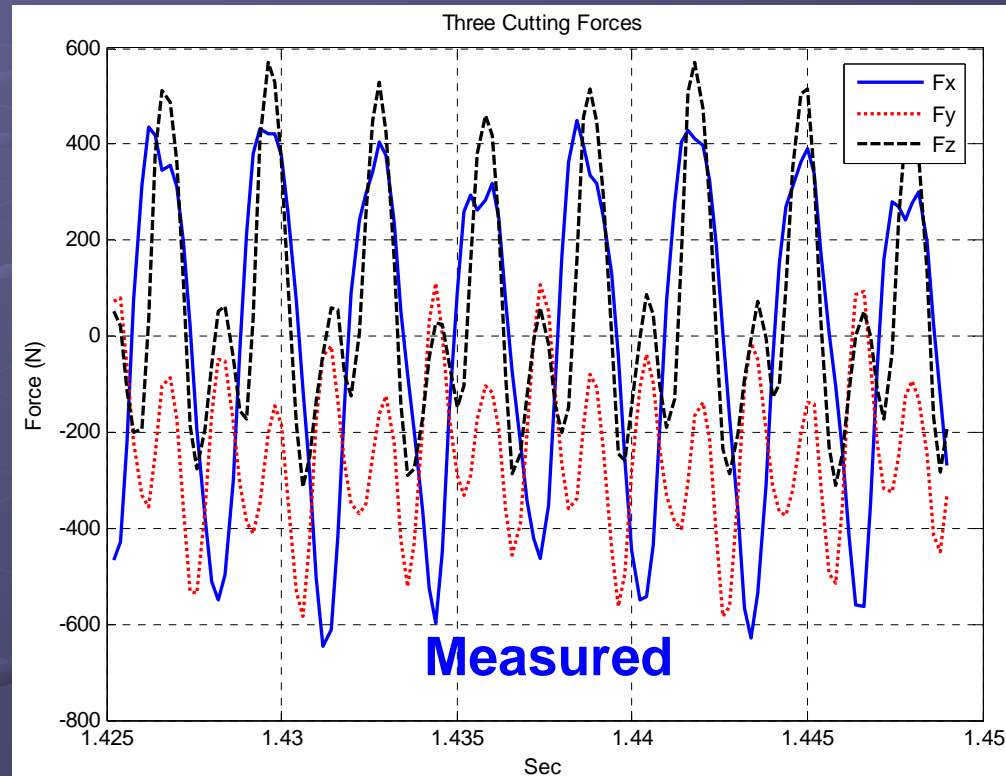
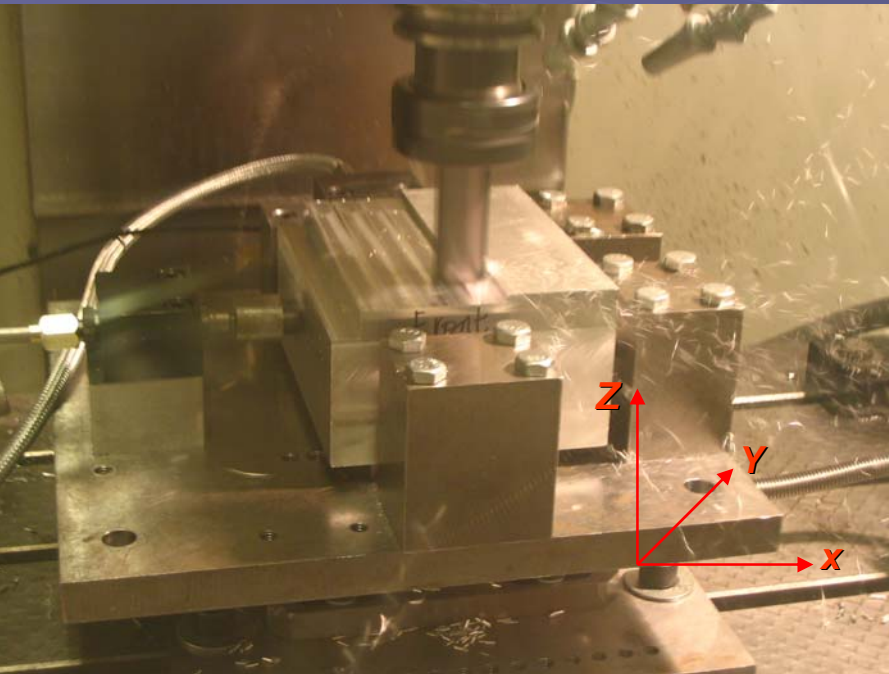
$FC = [1713.1, 1961.8, 1139.9] \text{ (N)}$

Experimental Validation (1)

Setup Schematic



Experimental Validation (2)



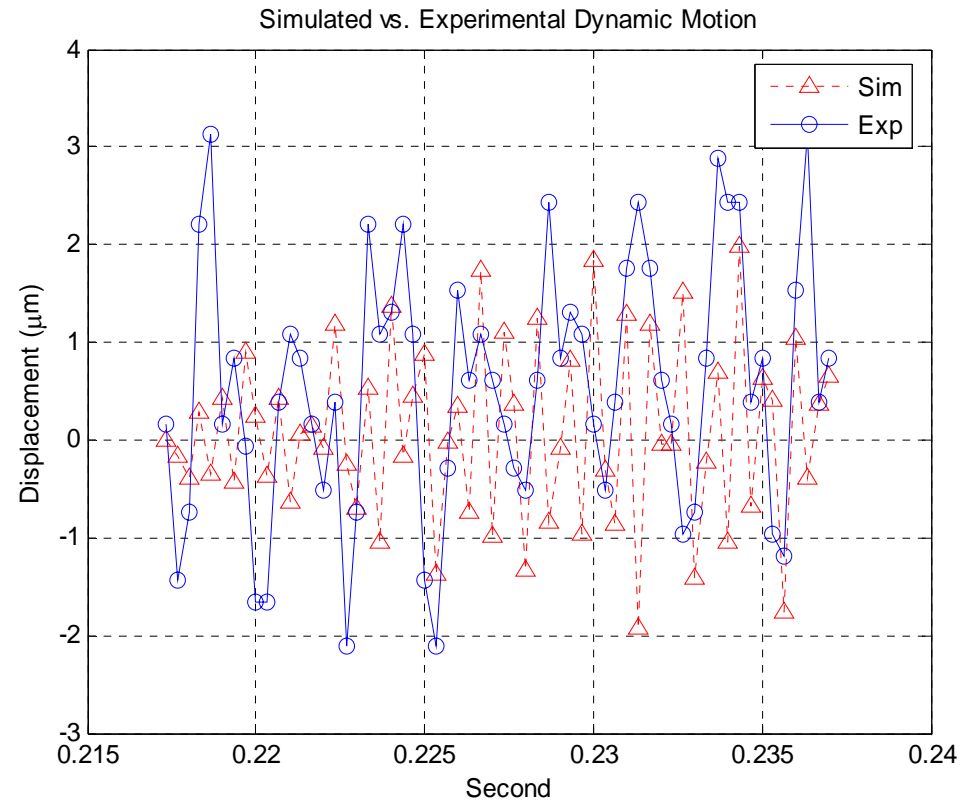
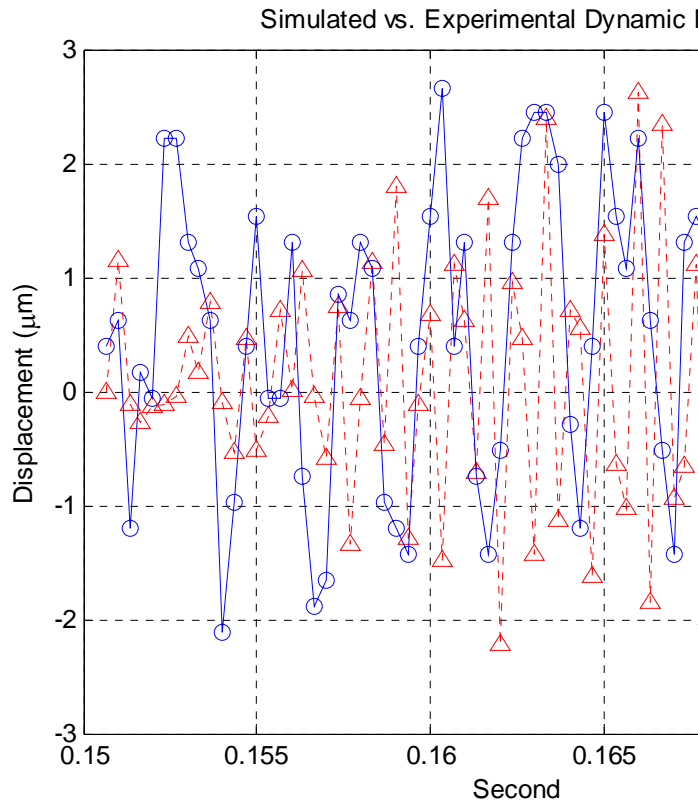
	Workpiece	Fixture Elements
Material	7075-T6 Aluminum	Hardened Steel
Density (kg/m^3)	2700	-
Young's modulus (GPa)	70.3	201
Poisson's ratio	0.354	0.296
Yield Strength (MPa)	500	-

Spindle Speed (rev/min)	Feed Rate (inch/min)	Axial Depth (inch)	Radial Depth (inch)	Clamping (psi)
5000	80	0.16	0.75	1500

(End mill: coated HSS, 1 inch, 4-flute)

Experimental Validation (3)

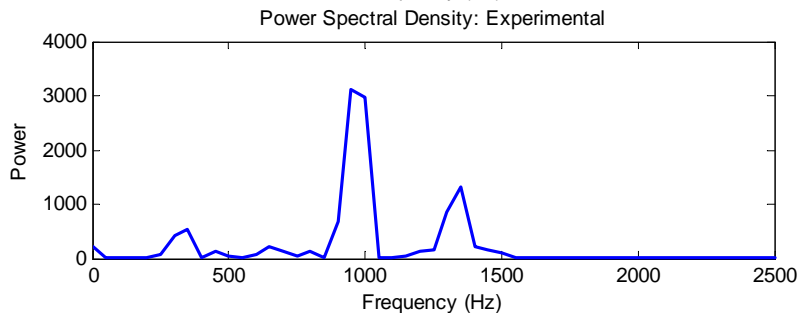
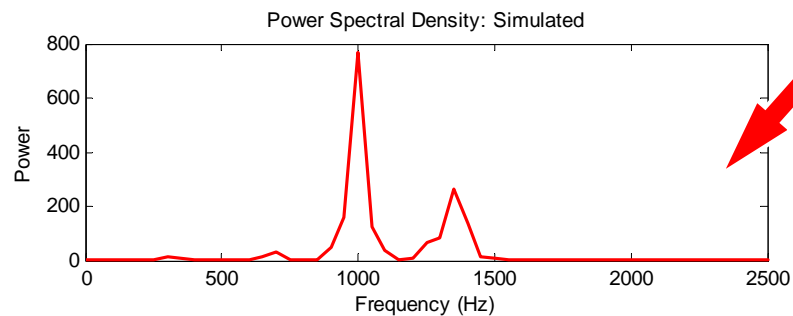
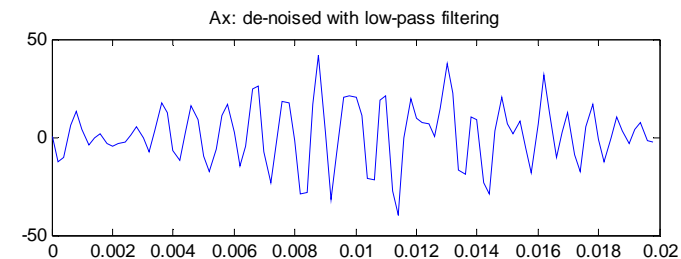
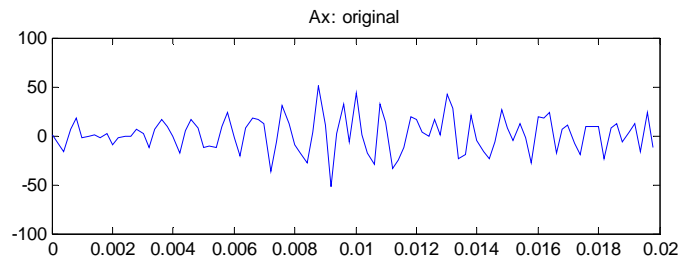
Sampling Rate = 3000 pts/sec



**Dynamic displacement of a surface point
measured by eddy current sensor**

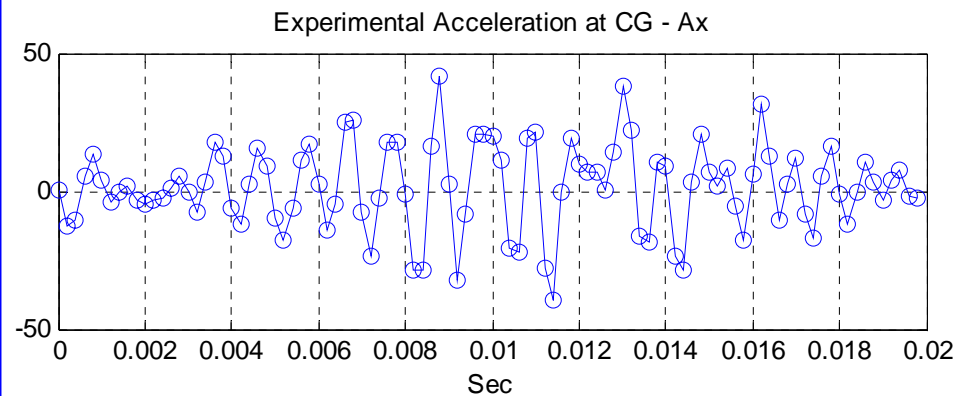
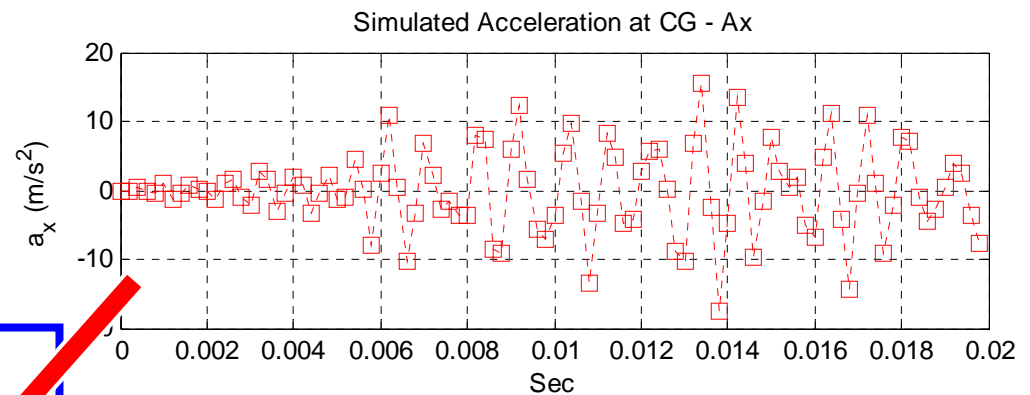
Acceleration – Data De-noising

Sampling Rate = 5000 pts/sec



Experimental Validation (4)

Acceleration @ CG: Simulated vs. Experimental



Conclusions

- A fixture-workpiece system presents significant dynamics during machining. Proper fixture design requires dynamic modeling.
- Material removal affects fixture-workpiece dynamics significantly.
- Dynamic motions of simulated and physical fixture-workpiece systems present similar frequency content.
- Experimental workpiece motion is larger than simulated workpiece motion because actual system is more flexible.

Acknowledgment

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